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# NASA Contractor Report 145277

## COMPUTATION OF THEORETICAL BRIGHTNESS TEMPERATURE CORRESPONDING TO THE CAPE CODE CANAL RADIOMETER MEASUREMENTS

(NASA-CR-145277) COMPUTATION OF THEORETICAL  
BRIGHTNESS TEMPERATURES CORRESPONDING TO THE  
CAPE COD CANAL RADIOMETER MEASUREMENTS  
Final Report (Wentz (Frank J.) and  
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N78-13716

Unclass

CSCL 08J G3/48 55177



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NASA PURCHASE ORDER L-24420A



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COMPUTATION OF THEORETICAL BRIGHTNESS TEMPERATURES  
CORRESPONDING TO THE CAPE COD CANAL RADIOMETER MEASUREMENTS

Introduction

The potential of microwave radiometers on earth satellites to sense the sea-surface temperature and roughness on an all-weather basis has generated interest in theoretical models for sea brightness temperatures ( $T_B$ ). Wentz [1975] computed  $T_B$  from a two-scale scattering model and compared the results with Hollinger's [1971] radiometer measurements. Although the overall agreement was good, discrepancies did exist and were probably due in part to errors in specifying the input parameters for the  $T_B$  model. Also an incomplete correction for the antenna patterns could have contributed to the disagreements.

The extensive ground-truth data collected in conjunction with recent radiometer measurements of the Cape Cod Canal [Swift, 1974] and the improved determination of the permittivity of saline water [C. T. Swift, private communication, 1975] now allow for a more accurate specification of the  $T_B$  model's input parameters. In addition, Beck [1975] has computed the corrections to  $T_B$  resulting from the Cape Cod Canal radiometer antenna patterns. In this report these investigations are used to take a closer look at the  $T_B$  model. First the input parameters are determined from the ground-truth data, and then the computations are compared with the radiometer measurements.

Input Parameters

The  $T_B$  model developed by Wentz [1975] requires the following inputs.

Operational Parameters

1. Radiometer frequency  $f$
2. Radiometer polarization  $P$
3. Radiometer viewing angle  $\theta$

### Environmental Parameters

1. Water surface temperature  $T_w$
2. Water salinity  $s$
3. Power spectrum  $S(\kappa)$  of the water surface,  $\kappa$  = wavenumber
4. Downward sky  $T_B$  angular distribution  $T_S(\theta_z)$ ,  $\theta_z$  = zenith angle

The operational parameters for the Cape Cod Canal measurements are  $f = 1.4$ , 4.0, and 7.5 GHz;  $P$  = horizontal and vertical; and  $\theta$  ranging from  $20^\circ$  to  $70^\circ$ . Computations are done at the three frequencies, two polarizations, and for  $\theta$  from  $0^\circ$  to  $70^\circ$  in  $10^\circ$  steps.

Two environmental cases are considered: one between the hours of 1840 and 1852 EDT on May 25, 1972, during which the canal's surface was rough, and the other between the hours of 0126 and 0138 EDT on May 26, 1972, during which the canal's surface was smooth. The ground-truth data required by the model are given in Table 1 for each case.

Table 1. Ground-Truth Data

|                              | Rough Surface | Smooth Surface |
|------------------------------|---------------|----------------|
| Water Temperature            | 286.1°K       | 283.9°K        |
| Water Salinity               | 28 ‰          | 28 ‰           |
| Air Temperature <sup>1</sup> | 282.6°K       | 279.8°K        |
| Wind Speed <sup>1</sup>      | 14 m/s        | 6 m/s          |

<sup>1</sup>Measured approximately 58 m above the canal surface

### Permittivity of the Canal Water

The permittivity  $\epsilon$  of saline water is a function of the water temperature  $T_w$ , salinity  $s$ , and frequency  $f$ . Swift's [private communication, 1975] expressions for  $\epsilon(T_w, s, f)$ , which are based in part on the waveguide measurements of Ho and Hall [1973], are used, and the results are given in Table 2.

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Table 2. Permittivity of Canal Water

| Frequency | Rough Surface  | Smooth Surface |
|-----------|----------------|----------------|
| 1.4 GHz   | 75.40 - 50.37J | 75.91 - 48.02J |
| 4.0 GHz   | 70.09 - 33.94J | 69.91 - 34.41J |
| 7.5 GHz   | 59.56 - 36.87J | 58.34 - 37.73J |

### Power Spectrum of the Canal Surface

The smooth surface was described as slick, and the wavestaff record was virtually level. In view of this, a specular surface is assumed for the smooth-surface computations. The rough-surface computations require that the surface power spectrum be specified. Information about the directional properties of the power spectrum of a wind-driven water surface is scarce, especially for a canal with an appreciable current, and the simplifying assumption that the spectrum is isotropic is made. Although the assumption is unrealistic, the anisotropies will probably tend to average out because the  $T_B$  computations involve integrations over all scatter directions.

The isotropic power spectrum  $S(\kappa)$  for  $\kappa \leq 10^{-3} \text{ cm}^{-1}$  was measured by a laser profilometer and by a wavestaff. However, this spectral region is unimportant to the  $T_B$  model because it contributes negligibly to the surface slope variance. The important part of the spectrum is  $\kappa > 10^{-3} \text{ cm}^{-1}$  for which no ground-truth spectral data is available. In order to specify  $S(\kappa)$  in this region, the friction velocity  $u_*$  corresponding to a 14 m/s wind in a neutral atmosphere at 58 m above the surface is calculated from expressions given by Cardone [1969]. The result,  $u_* = 51 \text{ cm/s}$ , is then inputted into Pierson and Stacy's [1973] expressions for the power spectrum of capillary waves (Eqs. 2.7, 2.8, and 2.9 in their report). In this way  $S(\kappa)$  is determined for  $\kappa \geq 0.359 \text{ cm}^{-1}$ . One should note that Cardone's expressions are for an open sea and the Pierson-Stacy expressions are based on wave tank measurements. Applying these expressions to a canal possibly introduces significant error.

The capillary power spectrum is connected to the ground-truth power spectrum by drawing a straight line on a  $\log S(\kappa)$  versus  $\log \kappa$  plot. This results in the following expressions:

$$S(\kappa) = S(\kappa_1) (\kappa_1/\kappa)^d \quad \text{for } \kappa_1 < \kappa < \kappa_2 \quad (1)$$

$$d = \log[S(\kappa_1)/S(\kappa_2)] / \log(\kappa_2/\kappa_1) \quad (2)$$

$$\kappa_1 = 10^{-3} \text{ cm}^{-1} \quad (3)$$

$$\kappa_2 = 0.359 \text{ cm}^{-1} \quad (4)$$

$$S(\kappa_1) = 1.2 \times 10^3 \text{ cm}^3 \quad (\text{laser profilometer}) \quad (5)$$

$$S(\kappa_2) = 0.372 \text{ cm}^3 \quad (\text{Pierson-Stacy}) \quad (6)$$

The spectrum for  $\kappa < 10^{-3} \text{ cm}^{-1}$  can be empirically found from the laser profilometer data, but this is not necessary because inspection shows that this portion of the spectrum contributes less than  $10^{-5}$  to the slope variance.

The treatment of two-scale scattering requires that  $S(\kappa)$  be divided into a large-scale spectrum  $S_\ell(\kappa)$  and a small-scale spectrum  $S_s(\kappa)$ .

$$S_\ell(\kappa) = \begin{cases} S(\kappa) & \kappa \leq \kappa_c \\ 0 & \kappa > \kappa_c \end{cases} \quad (7)$$

$$S_s(\kappa) = \begin{cases} 0 & \kappa \leq \kappa_c \\ S(\kappa) & \kappa > \kappa_c \end{cases} \quad (8)$$

The cutoff wavenumber  $\kappa_c$  is fixed by requiring that the rms height  $\zeta$  of the small-scale spectrum equals  $(4k)^{-1}$ , where  $k$  denotes the radiation wavenumber. Wentz [1975] showed that variations in the perturbation parameter  $k\zeta$  from 0.125 to 0.25 only slightly affects the  $T_B$  computations. Once  $\kappa_c$  is found the slope variance  $\sigma^2$  of the large-scale spectrum is calculated by integrating  $\kappa^2 S_\ell(\kappa)$  from  $\kappa = 0$  to  $\kappa = \kappa_c$ . Table 3 gives the values of  $\kappa_c$  and  $\sigma^2$  for the three frequencies.

Table 3. Cutoff Wavenumber and Large-Scale Slope Variance

| Frequency | Cutoff Wavenumber $\kappa_c$         | Large-Scale Slope Variance $\sigma^2$ |
|-----------|--------------------------------------|---------------------------------------|
| 1.4 GHz   | $2.4 \times 10^{-2} \text{ cm}^{-1}$ | $1.3 \times 10^{-4}$                  |
| 4.0 GHz   | $3.6 \times 10^{-1} \text{ cm}^{-1}$ | $1.1 \times 10^{-2}$                  |
| 7.5 GHz   | $7.7 \times 10^{-1} \text{ cm}^{-1}$ | $2.7 \times 10^{-2}$                  |

### Downward Sky Brightness Temperature

The following expressions for the downward sky  $T_B$  angular distribution  $T_s(\theta_z)$  are used in the model:

$$T_s(\theta_z) = (1-\tau)T_{\text{eff}} + \tau T_{\text{cos}} \quad (9)$$

$$\tau = (1 - T_{\text{zen}}/T_{\text{eff}})^{A(\theta_z)} \quad (10)$$

$$T_{\text{eff}} = 1.12 T_{\text{air}} - 50 \quad (11)$$

where  $T_{\text{air}}$  is the air temperature given in Table 1,  $T_{\text{zen}}$  is the zenith atmospheric  $T_B$ ,  $T_{\text{cos}}$  is the cosmic  $T_B$ , and  $A(\theta_z)$  is the air mass function [Allen, 1963]. The above equations are the same as given by Peake [1969] except that the exponent  $A(\theta_z)$  is used in place of  $\sec \theta_z$ .

Clear skies prevailed during the radiometer measurements, and Porter and Wentz's [1971] values for  $T_{\text{zen}}$  for a standard mid-latitude clear sky model are used and are given in Table 4. The cosmic  $T_B$  is the sum of the galactic  $T_B$  and the 2.7°K residual  $T_B$  of the primeval fireball. The spatial variation of the galactic  $T_B$  is quite large. Excluding discrete sources, the galactic center is about 35 times as bright as the cold sky for the frequencies being considered [Allen, 1963]. The cold sky is assumed, and the values for the galactic  $T_B$  and the cosmic  $T_B$  are shown in Table 4. Table 5 gives  $T_s(\theta_z)$  for the three frequencies and for the rough-surface case. The smooth-surface values are essentially the same because the 3 K° difference in air temperature between the two environmental cases results in a change in  $T_s(\theta_z)$  of only a few tenths of a K°.



Table 4. Input Parameters for the Sky Brightness Temperature Model

| Frequency | Zenith Atmospheric $T_B$ | Galactic $T_B$ | Cosmic $T_B$ |
|-----------|--------------------------|----------------|--------------|
| 1.4 GHz   | 2.2°K                    | 0.5°K          | 3.2°K        |
| 4.0 GHz   | 2.5°K                    | 0.0°K          | 2.7°K        |
| 7.5 GHz   | 2.9°K                    | 0.0°K          | 2.7°K        |

Table 5. Downward Sky Brightness Temperature Angular Distribution

| Zenith Angle $\theta_z$<br>deg | $T_S(\theta_z) - ^\circ K$ |         |         |
|--------------------------------|----------------------------|---------|---------|
|                                | 1.4 GHz                    | 4.0 GHz | 7.5 GHz |
| 0                              | 5.4                        | 5.2     | 5.6     |
| 5                              | 5.4                        | 5.2     | 5.6     |
| 10                             | 5.4                        | 5.2     | 5.6     |
| 15                             | 5.5                        | 5.3     | 5.7     |
| 20                             | 5.5                        | 5.3     | 5.8     |
| 25                             | 5.6                        | 5.4     | 5.9     |
| 30                             | 5.7                        | 5.6     | 6.0     |
| 35                             | 5.9                        | 5.7     | 6.2     |
| 40                             | 6.0                        | 5.9     | 6.4     |
| 45                             | 6.3                        | 6.2     | 6.7     |
| 50                             | 6.6                        | 6.5     | 7.2     |
| 55                             | 7.0                        | 7.0     | 7.7     |
| 60                             | 7.5                        | 7.6     | 8.4     |
| 65                             | 8.3                        | 8.5     | 9.4     |
| 70                             | 9.5                        | 9.8     | 11.0    |
| 75                             | 11.4                       | 12.0    | 13.5    |
| 80                             | 15.2                       | 16.3    | 18.4    |
| 85                             | 25.1                       | 27.5    | 31.2    |
| 90                             | 74.4                       | 82.1    | 92.4    |

#### Correction for Antenna Patterns

The radiometer measurements reported by Swift [1974] are antenna temperatures  $T_A$ ; that is, they are convolutions of  $T_B$  and the antenna gain patterns. Recent calculations by Beck [1975] show that the averaging effect of the antenna pattern produces significant differences between  $T_A$  and  $T_B$ . These differences,  $\Delta T = T_A - T_B$ , for the smooth surface are given in Table 6. Calculations were not done for  $\theta = 0^\circ$  or  $10^\circ$ , and  $\Delta T$  is assumed zero for these angles.

Furthermore  $\Delta T$  is assumed independent of the environmental parameters, and the values in Table 6 are also used in the rough-surface computations. The effect of the antenna patterns on  $T_B$  is accounted for by adding  $\Delta T$  to the  $T_B$  model computations.

Table 6. Antenna Pattern Corrections

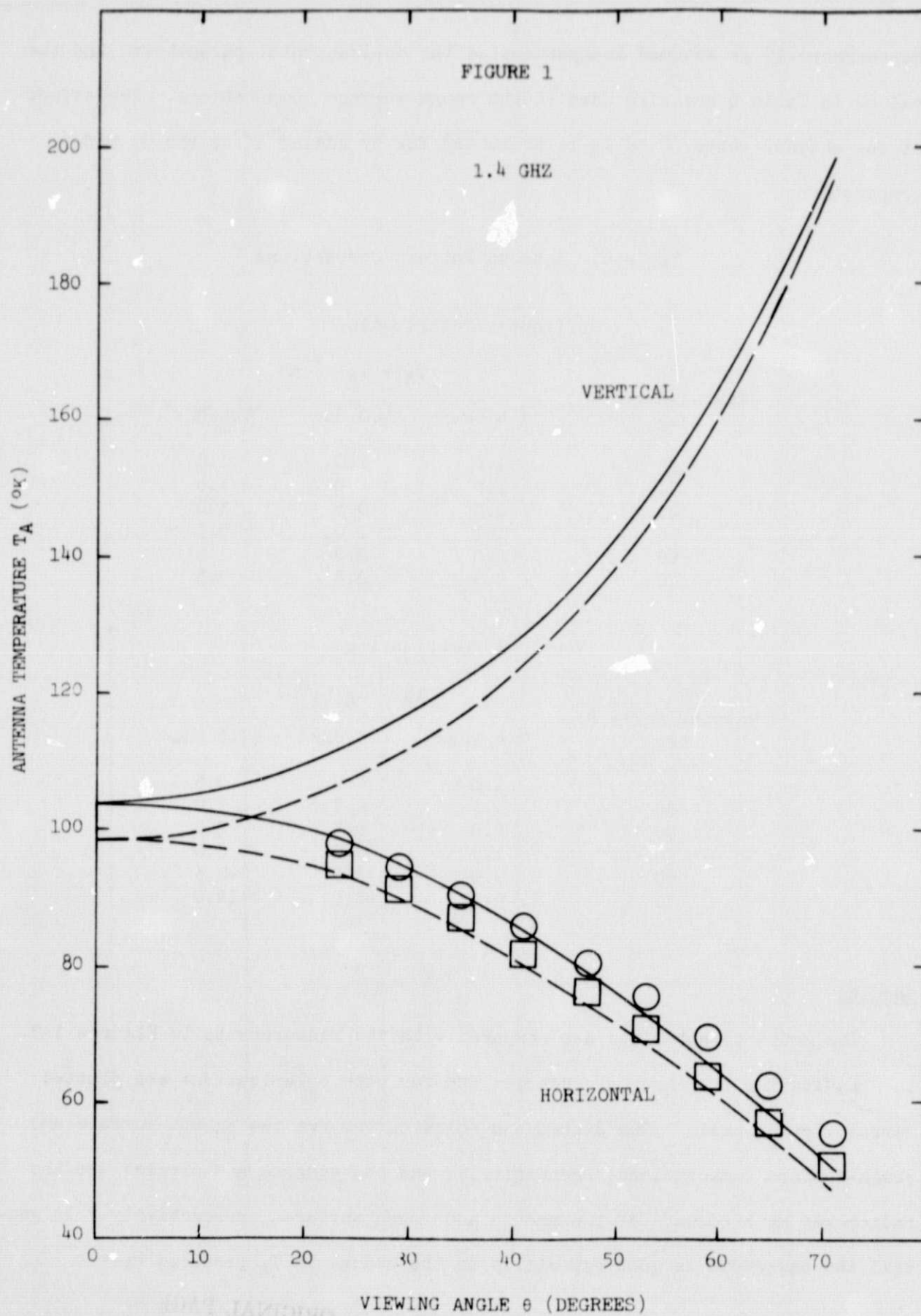
| Horizontal Polarization       |                                    |         |         |  |
|-------------------------------|------------------------------------|---------|---------|--|
| Viewing Angle $\theta$<br>deg | $T_A - T_B$ ( $^{\circ}\text{K}$ ) |         |         |  |
|                               | 1.4 GHz                            | 4.0 GHz | 7.5 GHz |  |
| 20                            | 1.0                                | 1.0     | 1.0     |  |
| 30                            | 1.0                                | 1.0     | 1.0     |  |
| 40                            | 0.5                                | 0.5     | 1.0     |  |
| 50                            | 1.0                                | 1.0     | 0.5     |  |
| 60                            | 2.0                                | 2.0     | 1.5     |  |
| 70                            | 3.5                                | 2.5     | 3.5     |  |

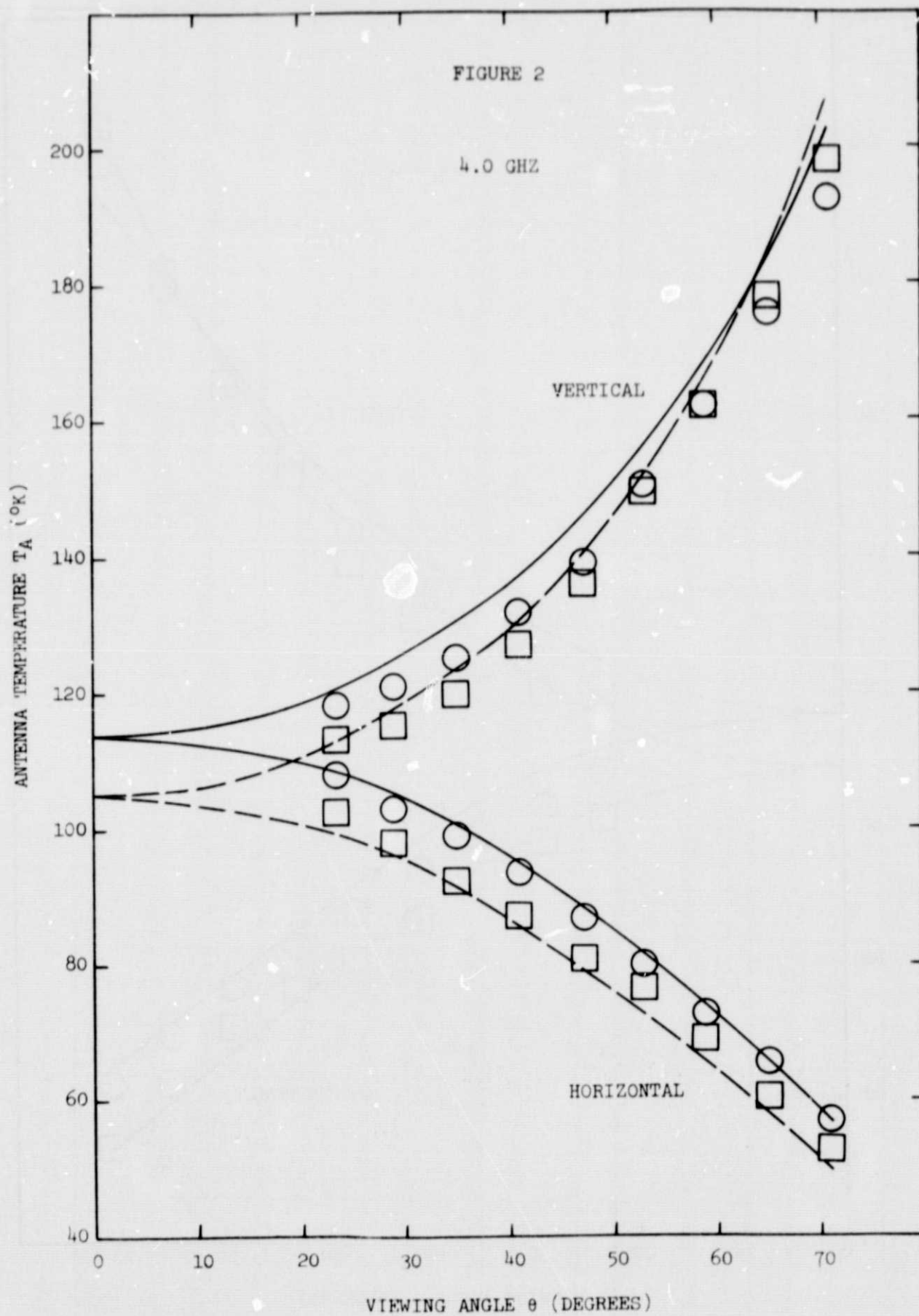
| Vertical Polarization         |                                    |         |         |  |
|-------------------------------|------------------------------------|---------|---------|--|
| Viewing Angle $\theta$<br>deg | $T_A - T_B$ ( $^{\circ}\text{K}$ ) |         |         |  |
|                               | 1.4 GHz                            | 4.0 GHz | 7.5 GHz |  |
| 20                            | 1.0                                | 0.5     | 0.5     |  |
| 30                            | 1.5                                | 0.5     | 1.0     |  |
| 40                            | 2.0                                | 0.5     | 2.0     |  |
| 50                            | 1.5                                | 0.0     | 0.0     |  |
| 60                            | 0.0                                | -2.5    | -2.5    |  |
| 70                            | -9.0                               | -8.0    | -14.0   |  |

### Results

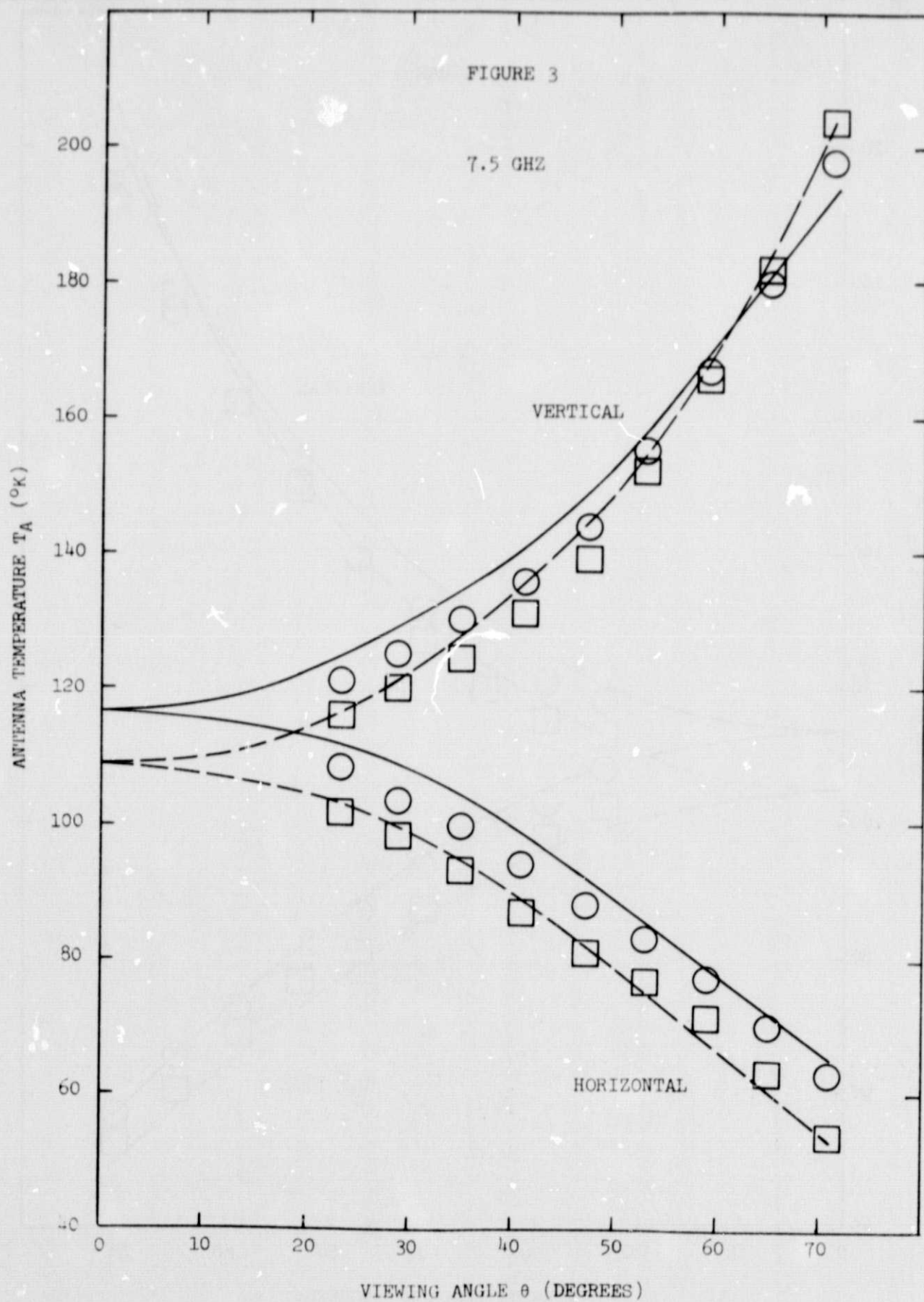
The model computations are compared with the measurements in Figures 1-3. The results for the three frequencies and for both polarizations are plotted versus viewing angle. The dashed and solid curves are the smooth-surface and rough-surface computations, respectively, and the squares and circles are the radiometer measurements of the smooth and rough surfaces, respectively. In general the agreement is good especially on the change in  $T_A$  produced by the

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presence of roughness. Discrepancies in magnitude do exist, but these are mostly less than twice the  $\pm 2$  K<sup>0</sup> error that is indicated by the size of the squares and circles. The agreement for horizontal polarization is somewhat better than for vertical polarization for which the computed  $T_A$  is greater than the measured  $T_A$  at intermediate viewing angles. The crossover of the smooth-surface and rough-surface curves for vertical polarization is in excellent agreement with the measurements at 7.5 GHz and in fair agreement at 4.0 GHz. No crossover occurs for the 1.4 GHz computations because essentially no large-scale roughness is present at this frequency as is indicated in Table 3.

Possible candidates contributing to the disagreements are listed below:

1. Error in specifying the power spectrum of the canal surface
2. Error in specifying the permittivity of the canal water, particularly at 1.4 GHz for which the permittivity is a strong function of the water temperature and salinity
3. Neglect of the large spatial variation of the galactic radiation at 1.4 GHz
4. Failure of the sky  $T_B$  model to consider atmospheric non-uniformities such as scattered clouds
5. Neglect of the contribution of the canal's shore to  $T_A$
6. Failure to use the total antenna pattern in computing  $T_A$
7. Neglect of intermediate-scale roughness by the two-scale scattering model
8. Experimental calibration error

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|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|-----------------------------|-------------------------------------------------------------------------------------|-------------------------------------------------------|--|
| 1. Report No.<br>NASA CR-145277                                                                                                                                                                                                                                                                            |                                                      | 2. Government Accession No. |                                                                                     | 3. Recipient's Catalog No.                            |  |
| 4. Title and Subtitle<br>Computation of Theoretical Brightness Temperatures<br>Corresponding to the Cape Cod Canal Radiometer Measure-<br>ments                                                                                                                                                            |                                                      |                             |                                                                                     | 5. Report Date<br>November 1977                       |  |
|                                                                                                                                                                                                                                                                                                            |                                                      |                             |                                                                                     | 6. Performing Organization Code                       |  |
| 7. Author(s)<br>Frank J. Wentz                                                                                                                                                                                                                                                                             |                                                      |                             |                                                                                     | 8. Performing Organization Report No.<br>Part I       |  |
| 9. Performing Organization Name and Address<br><br>Frank J. Wentz and Associates<br>Box 162, MIT Branch P.O.<br>Cambridge, MA 02139                                                                                                                                                                        |                                                      |                             |                                                                                     | 10. Work Unit No.                                     |  |
|                                                                                                                                                                                                                                                                                                            |                                                      |                             |                                                                                     | 11. Contract or Grant No.<br>L-24420A                 |  |
| 12. Sponsoring Agency Name and Address<br>National Aeronautics and Space Administration<br>Washington, D. C. 20546                                                                                                                                                                                         |                                                      |                             |                                                                                     | 13. Type of Report and Period Covered<br>Final Report |  |
|                                                                                                                                                                                                                                                                                                            |                                                      |                             |                                                                                     | 14. Sponsoring Agency Code                            |  |
| 15. Supplementary Notes                                                                                                                                                                                                                                                                                    |                                                      |                             |                                                                                     |                                                       |  |
| 16. Abstract<br><br>Theoretical brightness temperatures are computed from the ground-truth data that was collected during the radiometer measurements of the Cape Cod Canal. An approximate correction for antenna pattern effects is made, and the results are compared with the radiometer measurements. |                                                      |                             |                                                                                     |                                                       |  |
| 17. Key Words (Suggested by Author(s))<br><br>Microwave radiometer<br><br>Antenna temperature<br><br>Brightness temperature                                                                                                                                                                                |                                                      |                             | 18. Distribution Statement<br><br>Unclassified<br><br>Unlimited Subject Category 48 |                                                       |  |
| 19. Security Classif. (of this report)<br>Unclassified                                                                                                                                                                                                                                                     | 20. Security Classif. (of this page)<br>Unclassified | 21. No. of Pages<br>12      | 22. Price*<br>\$4.00                                                                |                                                       |  |